

An Introduction to PALM: Filtering – Filter methods

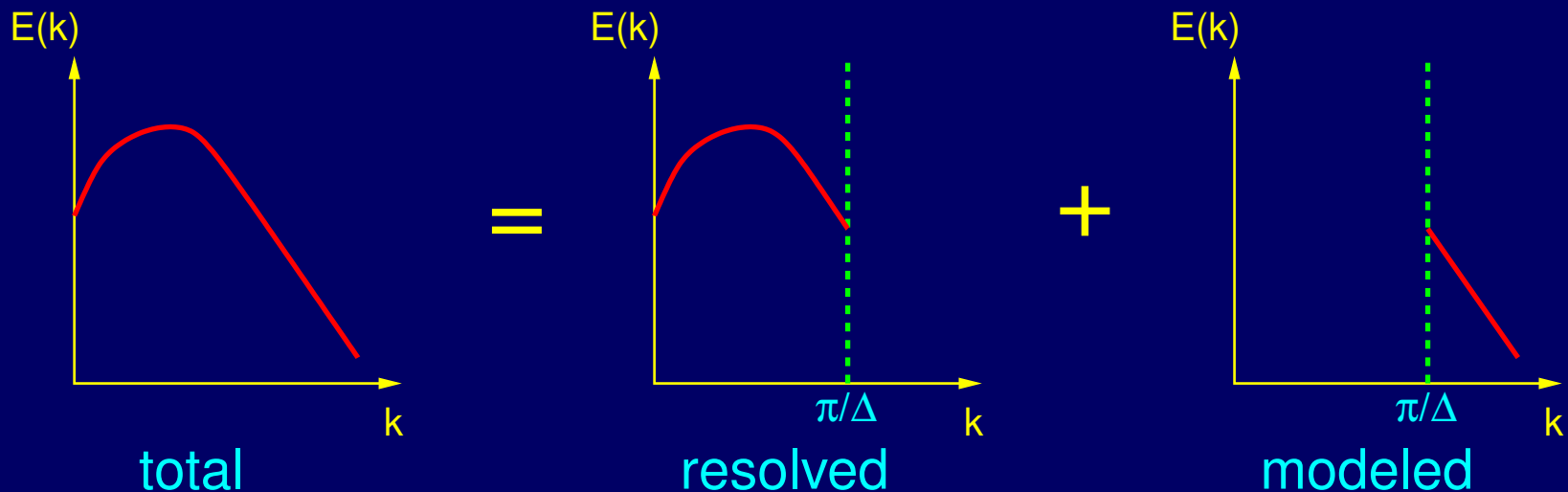
Zingst, July 10, 2003

Overview/Content

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- ② Theory of Scale Separation
- ③ Filtered Navier-Stokes Equations
- ④ Theory and Practice
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Introduction

- ⇒ The large-eddy simulation technique is based on scale separation, in order to reduce number of degrees of freedom of the solution
- ⇒ Low-frequency modes are calculated directly (resolved scales)
- ⇒ Small/subgrid/subfilter scales are parameterized by a way of a statistical model (sub-grid/sub-filter model)
- ⇒ These two categories of scales are separated by defining a cutoff length $\overline{\Delta}$



Theory of Scale Separation – Definitions

- ⇒ Formally the scales are separated by applying a low-pass filter to the exact solution
- ⇒ Filtering is mathematically represented by a convolution product in the physical space
- ⇒ the resolved part is formally defined by the relation:

$$\bar{\phi}(x_i, t) = \int_{-\infty}^{+\infty} dt' \int_{-\infty}^{+\infty} d^3x'_i \phi(x'_i, t') G(x_i - x'_i, t - t'), \quad (\bar{\phi} = G \star \phi)$$

with: G = convolution kernel

ϕ = exact solution for a space-time variable

- ⇒ The unresolved (modeled) part is defined as:

$$\phi'(x_i, t) = \phi(x_i, t) - \bar{\phi}(x_i, t), \quad (\phi' = (1 - G) \star \phi)$$

Theory of Scale Separation – Properties of the filter

⇒ The filter has to verify the following properties

① Conservation of constants:
$$\bar{a} = a \Leftrightarrow \int_{-\infty}^{+\infty} dt' \int_{-\infty}^{+\infty} d^3x'_i G(x'_i, t') = 1 .$$

② Linearity:
$$\overline{\phi + \psi} = \bar{\phi} + \bar{\psi} .$$

③ Commutation with derivation:
$$\overline{\frac{\partial \phi}{\partial s}} = \frac{\partial \bar{\phi}}{\partial s}, \quad s = x_i, t .$$

⇒ Filters verifying these properties are not, in the general case, Reynolds operators ($\overline{\bar{\phi}} = \bar{\phi}, \overline{\bar{\phi}'} = 0$):

$$\overline{\bar{\phi}} = G \star G \star \phi = G^2 \star \phi \neq \bar{\phi}$$

$$\overline{\bar{\phi}'} = G \star (1 - G) \star \phi \neq 0$$

Classical filters for Large-Eddy Simulation

☞ Box or "top-hat" filter:

$$G(x - x') = \begin{cases} \frac{1}{\bar{\Delta}} & \text{if } |x - x'| \leq \frac{\bar{\Delta}}{2} \\ 0 & \text{else} \end{cases}, \quad \tilde{G}(k) = \frac{\sin(k\bar{\Delta}/2)}{(k\bar{\Delta})/2}.$$

☞ Gaussian filter:

$$G(x - x') = \left(\frac{\gamma}{\pi\bar{\Delta}^2} \right)^{1/2} \exp\left(\frac{-\gamma |x - x'|^2}{\bar{\Delta}^2} \right), \quad \tilde{G}(k) = \exp\left(\frac{-\bar{\Delta}^2 k^2}{4\gamma} \right),$$

(The constant γ is generally taken to be 6)

☞ Spectral or sharp cutoff filter:

$$G(x - x') = \frac{\sin(k_c(x - x'))}{(k_c(x - x'))} \quad \text{with } k_c = \frac{\pi}{\bar{\Delta}}, \quad \tilde{G}(k) = \begin{cases} 1 & \text{if } |k| \leq k_c \\ 0 & \text{else} \end{cases}.$$

Filtered Navier-Stokes equations

⇒ Applying the filter to the Navier-Stokes equations lead to

Momentum equations:

$$\frac{\partial \bar{u}_i}{\partial t} + \frac{\partial}{\partial x_j} (\overline{u_j u_i}) = -\frac{1}{\rho_0} \frac{\partial \bar{p}}{\partial x_i} + \frac{g}{\theta_{v00}} (\bar{\theta}_v - \theta_{v00}) \delta_{i3} .$$

Equation of continuity:

$$\frac{\partial \bar{u}_i}{\partial x_i} = 0$$

Equations for scalar variables:

$$\frac{\partial \bar{\psi}}{\partial t} = -\frac{\partial (\overline{u_i \psi})}{\partial x_i}$$

⇒ The filtering process provides the non-linear terms, e.g. $\overline{u_j u_i}$,

⇒ In order for this equations to be usable the non-linear terms (e.g., $\overline{u_j u_i}$) have to be expressed as a function of the filtered quantities (e.g., \bar{u}_i) and of sub-filter scales (u'_i)

☛ This requirement leads to the approach of decomposing the non-linear terms

Decomposing the non-linear term – Leonard's decomposition (I)

⇒ Introducing the basic definition of filtered and sub-filter scales the non-linear term could be expressed as a triple summation:

$$\overline{u_i u_j} = \overline{(\bar{u}_i + u'_i)(\bar{u}_j + u'_j)} = \overline{\bar{u}_i \bar{u}_j} + \overline{\bar{u}_i u'_j} + \overline{\bar{u}_j u'_i} + \overline{u'_i u'_j}$$

⇒ Non-linear term is entirely written as a function of filtered and sub-filter scales (\bar{u}_i and u'_i)

⇒ Two versions of introducing this decomposition to the Navier-Stokes equations exist:

- ① Double decomposition (straight forward solution)
- ② Triple decomposition

Decomposing the non-linear term – Leonard's decomposition (II)

① Double decomposition

- ☞ This approach considers that all the terms appearing in the evolution equation of the filtered quantity must themselves be filtered quantities:

$$\frac{\partial \bar{u}_i}{\partial t} + \frac{\partial}{\partial x_j} (\overline{u_j u_i}) = -\frac{1}{\rho_0} \frac{\partial \bar{p}}{\partial x_i} + \frac{g}{\theta_{v00}} (\bar{\theta}_v - \theta_{v00}) \delta_{i3} - \frac{\partial \tau_{ij}}{\partial x_j}$$

with τ_{ij} being the sub-grid tensor

- ☞ τ_{ij} is grouping together terms that are not exclusively dependent on large scales:

$$\tau_{ij} = C_{ij} + R_{ij} = \overline{u_i u_j} - \overline{\bar{u}_i \bar{u}_j}$$

with $C_{ij} = \overline{u_i u'_j} + \overline{u'_j u_i} =$ cross-stress tensor

☞ Reflecting interactions of large and small scales

$R_{ij} = \overline{u'_i u'_j} =$ Reynolds sub-grid tensor

☞ Reflecting interactions between sub-grid scales

Decomposing the non-linear term – Leonard's decomposition (II)

② Triple decomposition

☞ Considers that it must be possible to evaluate the terms directly from the filtered variables

☞ $\overline{\overline{u_i u_j}}$ cannot be calculated directly, requires a second application of the filter

☞ Leonard proposes a further decomposition

$$\overline{\overline{u_i u_j}} = (\overline{\overline{u_i u_j}} - \overline{u_i u_j}) + \overline{u_i u_j} = L_{ij} + \overline{u_i u_j}.$$

☞ Defining τ_{ij} as

$$\tau_{ij} = L_{ij} + C_{ij} + R_{ij} = \overline{\overline{u_i u_j}} - \overline{u_i u_j}$$

leads to

$$\frac{\partial \overline{u_i}}{\partial t} + \frac{\partial}{\partial x_j} (\overline{u_j u_i}) = -\frac{1}{\rho_0} \frac{\partial \overline{p}}{\partial x_i} + \frac{g}{\theta_{v00}} (\overline{\theta_v} - \theta_{v00}) \delta_{i3} - \frac{\partial \tau_{ij}}{\partial x_j}$$

Decomposing the non-linear term

- ⇒ Beside the Leonard decomposition a more general approach exist: Germano consistent decomposition (not shown here)
- ⇒ For further information it is referred to Literature

Intermediary summary

- ⇒ The large-eddy simulation technique is a technique for reducing the number of degrees of freedom by separating the scales
- ⇒ The selection is made by a filtering technique (low-pass filter)
- ⇒ Two categories: resolved scales and sub-grid scales
- ⇒ The complexity of the solution is reduced by retaining only the large scales
- ⇒ The information concerning the small scales are grouped into the sub-grid tensor
- ⇒ In order for the dynamics of the resolved scales to remain correct, the sub-grid terms have to be considered ⇒ sub-grid models (see lecture sub-grid-scale models)

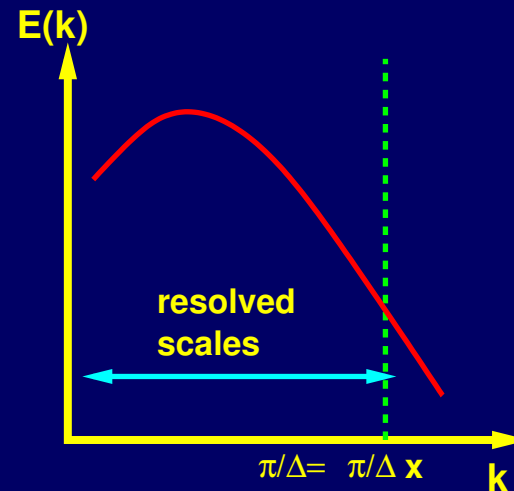
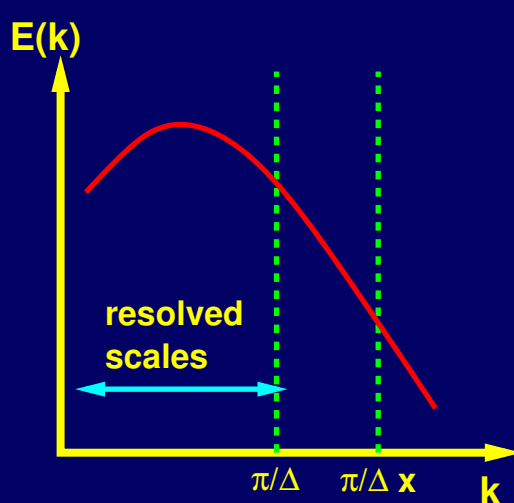
Theory and practice

- ⇒ The previous developments completely ignore the computational grid used for solving the Navier-Stokes equations numerically
- ⇒ The computational grid introduces another space scale: the discretization step Δx
- ⇒ Δx has to be small enough to be able to apply the filtering process correctly:

$$\Delta x \leq \bar{\Delta}$$

- ⇒ Two possibilities:

- ① Pre-filtering technique ($\Delta x < \bar{\Delta}$)
- ② Linking the analytical filter to the computational grid ($\Delta x = \bar{\Delta}$)



Theory and practice (II)

Pre-filtering:

- ⇒ Increases the number of degrees in the numerical solution without increasing the number of degree of freedom in the physically resolved solution
- ⇒ Requires that the analytical filter is performed explicitly
- ⇒ Rarely used in practice, due to additional computational costs

Linking the analytical filter to the computational grid:

- ⇒ The analytical cutoff length is associated with the grid spacing
- ⇒ This method does not require the use of an analytical filter
- ⇒ Brings some disadvantages concerning the evaluation of sub-grid models (should not be discussed further)
- ⇒ Because of its simplicity, this method is used by nearly all authors (e.g., see Schumann, 1975)

Interpretation of the LES

Understanding:

The energy spectrum of the computed solution has to verify the Kolmogorov spectrum modified by the transfer function of the filter

Kolmogorov spectrum: $E(k) = F(k^{-5/3})$
modified spectrum: $E(k) = F(k^{-5/3} \cdot \tilde{G}^2)$

Observation:

Applying a 'backward' filtering to the computed solution does not reproduce the exact solution

The comparison of spectra calculated from LES-data and theoretical spectra has shown significant differences

Reason:

Actually, the computed solution is the result of four filtering processes in total:

- ① The analytical filter, used to express the filtered Navier-Stokes equations
- ② A filter associated with the computational grid (frequencies larger than the Nyquist frequency cannot be represented in the simulation)
- ③ A filter induced by the numerical scheme (e.g., numerical diffusion of advection schemes)
- ④ A filter associated with the sub-grid model

Conclusion:

Details of the filtering process, especially the character of the filter-operator, are not known **a priori**, since the solution obtained by LES is a result of an additional implicit filtering operation

☞ **Actually, you don't know which filter function you are using!**

The final set of equations:

Equation of continuity:

$$\frac{\partial \bar{u}_i}{\partial x_i} = 0$$

Momentum equations:

$$\frac{\partial \bar{u}_i}{\partial t} = -\frac{\partial(\bar{u}_j \bar{u}_i)}{\partial x_j} - \frac{1}{\rho_0} \frac{\partial \bar{p}^*}{\partial x_i} - (\varepsilon_{ijk} f_j \bar{u}_k - \varepsilon_{i3k} f_3 u_{kgeo}) + \frac{g}{\theta_{v00}} (\bar{\theta}_v - \theta_{v00}) \delta_{i3} - \frac{\partial \tau_{ij}}{\partial x_j}$$

Liquid water potential temperature:

$$\frac{\partial \bar{\theta}_l}{\partial t} = -\frac{\partial(\bar{u}_i \bar{\theta}_l)}{\partial x_i} - \frac{\partial W_i}{\partial x_i} + \left(\frac{\partial \bar{\theta}_l}{\partial t} \right)_{\text{rad}} + \left(\frac{\partial \bar{\theta}_l}{\partial t} \right)_{\text{prec}}$$

Total water content:

$$\frac{\partial \bar{q}}{\partial t} = -\frac{\partial(\bar{u}_i \bar{q})}{\partial x_i} - \frac{\partial H_i}{\partial x_i} + \left(\frac{\partial \bar{q}}{\partial t} \right)_{\text{prec}}$$

$$\tau_{ij} = \overline{u_j u_i} - \bar{u}_j \bar{u}_i$$

$$H_i = \overline{u_i \theta_l} - \bar{u}_i \bar{\theta}_l$$

$$W_i = \overline{u_i q} - \bar{u}_i \bar{q}$$

explicitly solved

parameterized (sub-grid model)

implicitly achieved

Literature

Sagaut, P, 2001: Large eddy simulation for incompressible flows: An introduction. — Springer Verlag, Berlin/Heidelberg/New York, 319 p.

Schumann, U., 1975: Subgrid scale model for finite difference simulations of turbulent flows in plane channels and annuli. — J. Comp. Phys., **18**, 376–404